BTX Extractive Distillation Capacity
Increased by Enhanced Packing Distributors

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Table of Contents

1. Abstract 3
2. Background 4
3. Opportunities Found in May 2000 5
4. Tower Problem Solving 7
5. July 2000 Test Run 8
6. January 2001 Turn Around 9
7. The Extractive Distillation Column 11
8. May 2001 Test Run 16
9. Lessons Learned 16
10. Conclusions 17
Abstract

A new grassroots BTX Extractive Distillation Unit was commissioned in February 2000. A test run was performed in July 2000 and plant design criteria was marginally accomplished. A review of the tower internals was completed and recommendations made to improve the distributors and reduce the area of the distributor supports that obstructed the packing.

In January 2001, with the turn around of the Ethylene Cracker, the recommended modifications were installed. With the modifications to the distributors and retraying a limiting stripping section, all the plant design criteria were met. Additionally an 18% increase in aromatic production capacity was achieved while improving aromatic recoveries. Enhanced distributors can greatly improve the fractionation capacity of structured packing.
**Background**

A grass roots extractive distillation BTX unit was commissioned in January 2000. The unit consisted of a Reactor Pretreatment Section, an Extractive Distillation (ED) Column, a Stripper Column, and a Benzene-Toluene Distillation Column. The ED Column has four structured packed sections in the rectifying section (top of the tower) and trays in the stripping section (bottom of the tower). The Stripper Column has one structured packed bed with one tray in the rectifying section and trays in the stripping section.

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**ED Column**

**Stripper Column**
After commissioning the unit failed to meet design rates and recoveries. The operation was reviewed and it was decided that new Z-Bar type trays, with small slotted valves, in the bottom of the ED Tower would meet design conditions. Z-Bar trays have additional area in the downcomer to allow more liquid traffic. Small slotted valves, which are smaller than standard valves, have higher overall efficiency. The unit was shut down in May 2000 for tray replacement.

**Opportunities Found in May 2000**

The team of maintenance and engineering personnel, that included some of the authors, was able to inspect the ED Column and Stripper Column in May 2000. The columns were found to be clean and well constructed. The design was similar to those that the technology licensee had utilized in the past with success. It is acceptable to utilize past designs only if they conform to basic engineering fundamentals.

The first opportunity found was at the top of the third bed of the ED Column, counting from the top down. This was the lean solvent feed point. The liquid distributor had two issues. The first issue was that four by eight inch plates on top of the packing supported the distributor. These plates covered 8% of the packing. Packing loses its efficiency by channeling. Channeling is when the vapor and liquid travel in separate paths and fail to mix. Channeling can present itself in two phenomena; one in macro and one in micro.

The micro phenomenon is in the point flow. As the liquid travels down the length of the packing bed less and less mixing occurs leading to reduced heat and mass transfer. The liquid coalesces into large flow streams by passing the rising vapor. A four by eight-inch plate blocks the rising vapor flow and sets up a channeling regimen, negating the effect of the distributor. The plates are blocking the gas flow underneath and the vapor below the plates is channeled to the side. A reduced separation or heat exchange efficiency is induced and column capacity may be reduced.

The macro phenomenon is in the bulk flow. One half of the liquid is on the left side of the column and one half is on the right. If the liquid is not collected and re-mixed between the beds, a bulk flow composition difference can exist between the right and left side of the column.

The second opportunity was in the distributor itself. At this point the distributor had two feeds. The first was from the second bed of packing, which was mostly hydrocarbon, and the second was from the lean solvent feed point. The distributor was essentially two distributors in parallel; no pre mixing of the feeds to the third bed was preformed. This meant that the hydrocarbon from the second bed and the lean solvent did not begin to contact until several feed down the bed of the packing.
The third opportunity found was at the bottom of the third bed. The bottom of the third bed did not have a liquid collector. Liquid was allowed to freely rain down on next chimney tray, setting up the macro phenomena. A liquid collector and distributor has two functions. First is to collect, mix the liquid, and route it to the next bed.

The second is to evenly distribute the vapor across the upper bed section. In some cases without a collector, the vapor may be channeled leading to reduced packing efficiency. Vapor distribution is required; 1) if there is not sufficient height between the beds for vapor mixing, 2) at high-pressure applications where gas densities are high, and 3) where there is a small gas to liquid density ratio.

The fourth opportunity found was on the fourth bed. The fourth bed’s distributor was a chimney tray. At this point there are two liquid phases, hydrocarbon and solvent. A standard chimney tray may not be the best distributor for two liquid phases with different densities.

The fifth and last opportunity found was that the fourth bed did not have a hold down grid below the chimney tray. Hold down grids maintain the levelness of the packing during a mild column upset, reducing channeling. The packing appeared to be miss-aligned under the chimney tray.

Recommendations were made to rectify each of the items mentioned, but due to time constraints decisions were made to only redistribute the upset packing and replace the bottom 37 trays with enhanced liquid and vapor capacity trays. The unit was then recommissioned.

**Turn Around Time Management**

In a turn around, decisions are normally made quickly in view of lost production, with the hope that the shortest most reasonable outage will result in improved tower performance. It is difficult when a unit is down and no sellable products are being produced to extend an outage. The unit manager has to balance the cost of an additional day or days of lost production versus the potential gain of improved tower performance. It is often difficult to quantify the potential gain of the improved tower performance.

It is very important for a decision-maker to have considered what some of the potential scenarios they could encounter before the turn around begins. Some of the scenarios that may cause additional time in the outage include; 1) damaged trays, 2) upset packing, 3) damaged feed / reflux nozzles, 4) improper installation, and 5) design deviating from basic principles.

Managers are group leaders that bring teams of people together for the best overall result. It is important for managers to built relationships, in advance of problems, with competent distillation engineers so that the potential gain of improved tower performance can be quantified quickly with reliability. With the ability to transfer information quickly, many decisions can be made with reliable guidance.
**Tower Problem Solving**

The first step in resolving any distillation problem is to understand the operating and technical fundamentals of the column. Knowledge of how a column functions, hydraulic constraints, thermodynamic and equilibrium limits, and heat and material balances are required. This knowledge needs to be accumulated in advance of formulating any resolution of a problem.

At least four types of distillation equipment problems can exist. The first problem is inappropriate design, the second is inappropriate installation, the third is inappropriate operation, and the fourth is potential damage to internal equipment. Before a process is shut down for repairs the inappropriate design and damage to internal equipment should be determined, and inappropriate operation should be eliminated.

**Synopsis of Tower Troubleshooting**

Always do simple checks first.

1. Ensure that levels are accurate. Have operations move levels and view changes in the field.
2. Calculate column pressure drop and then measure pressure drop. Review survey pressure reading to operation’s readings.
3. Survey column temperature profile. Review survey temperature reading to operation’s readings.

**Verify Tower Operations**

Perform tower simulation to verify Tower Stage efficiency. Sometimes the feed compositions changes and tower is no longer able to meet desired specifications due to thermodynamic or equilibrium constraints. Parameters required to perform the simulation will be:

1. Accurate tower feed, Overhead, and Bottoms laboratory analysis
2. Accurate tower mass balance, within 2%.
3. Heating and cooling medium temperatures.

If the tower simulation confirms the limits are not beyond thermodynamic or equilibrium constraints and additional check may be to have the tower gamma scanned to look for tray damage. This type of troubleshooting method can determine internal damage, vapor liquid mal-distribution, and packed and trayed tower fouling. Because of economic constraints, scanning should be chosen only after the simple checks and the limits are confirmed. Scanning can sometimes confirm the problem that was identified by the other checks.
July 2000 Test Run

From May to July the unit was further optimized. Several other non-distillation unit issues were resolved. During July 13th through the 16th a unit test run was performed. The unit was able to test run design rates, but did not meet benzene recoveries. Benzene design recovery was 97.0 wt % and Toluene design recovery was 98.0 wt %.

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<tr>
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<th>Test Run Design</th>
<th>13 July 00</th>
<th>14 July 00</th>
<th>15 July 00</th>
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From July until December the unit was operated and additional optimization was performed.

November High Load Test

During November a high load test was conducted to determine the existing limits of each section of the plant. A properly planned and executed high load test can provide valuable information in unit revamps. A high load test can provide insight into the unit’s current problems and under utilized equipment.

The feed was raised step wise, over a two-day period, November 10th and 11th, to test each section. The feed rate was slowly raised to 123% as a hydraulic system check neglecting product recoveries. The limiting section of the plant was found to be the Stripper Column, which had solvent carry over at 111%.
January 2001 Turn Around

During the January 2001 turn around the opportunity was taken to upgrade the BTX Unit. Simulations were conducted rate the ED and Stripper Column. The existing packing in the ED and Stripper Column was rated at 140% of design. The new trays in the bottom of the ED Column were rated at 125% of design.

The unit limits were found to be the distributors and the Stripper Column trays. An additional consideration was the solvent carry over in the Stripper Column. The Stripper Column had one tray and a large, twenty plus foot, packed bed above the feed point to reduce solvent losses. Reflux was washed down the packed bed to remove the solvent from the aromatics. One would not expect that the solvent would carry over with the overhead vapor from a large packed bed.

The Stripper Column

To reduce the solvent carry over, the top tray below the packed bed was converted to a chimney tray. A small amount of fractionation capacity was lost, but during the high load test the aromatics in the lean solvent had remained low. Chimney tray design seems straight forward, but several factors need to be considered in the design. The pressure drop of the chimney tray needs to be reviewed, and minimized if possible, as this tray does no actual fractionation. The vapor distribution needs to be reviewed and redistributed if necessary by the design of the chimney hats.

Schematic of new Chimney Tray
The remaining Stripper Column trays were upgraded to the Z-Bar style with small valves to match the ED Column trays. They were rated to 140% of design. One negative of raising tower tray rates is the column down turn, or minimum rates. By increasing the design rating to 140%, the new effective column minimum-operating rate was raised.